## Thick-Film Hybrid IC

## STK412-150C-E - Two-Channel Power Switching System Audio Power IC, 150W+150W

## Overview

The STK412-150C-E is a class H audio power amplifier hybrid IC that features a built-in power supply switching circuit. This IC provides high efficiency audio power amplification by controlling (switching) the supply voltage supplied to the power devices according to the detected level of the input audio signal.

## Applications

- Audio power amplifiers.


## Features

- High output power by using power MOSFETs.
- Output load impedance: $\mathrm{R}_{\mathrm{L}}=8 \Omega$ to $6 \Omega$ supported
- Using insulated metal substrate that features superlative heat dissipation characteristics that are among the highest in the industry.


## Series Models

|  | STK412-150C-E | STK412-170C-E |  |
| :--- | :---: | :---: | :---: |
| Output $(0.7 \% / 20 \mathrm{~Hz}$ to 20 kHz$)$ | $150 \mathrm{~W} \times 2$ channels $\left(\mathrm{R}_{\mathrm{L}}=6 \Omega\right)$ | $180 \mathrm{~W} \times 2$ channels $\left(\mathrm{R}_{\mathrm{L}}=4 \Omega\right)$ |  |
| Max. rated $\mathrm{V}_{\mathrm{H}}$ (quiescent) | $\pm 95 \mathrm{~V}$ | $\pm 95 \mathrm{~V}$ |  |
| Max. rated $\mathrm{V}_{\mathrm{L}}$ (quiescent) | $\pm 61 \mathrm{~V}$ | $\pm 60 \mathrm{~V}$ |  |
| Recommended operating $\mathrm{V}_{\mathrm{H}}$ | $\pm 57 \mathrm{~V}$ | $\pm 54 \mathrm{~V}$ |  |
| Recommended operating $\mathrm{V}_{\mathrm{L}}$ | $\pm 38 \mathrm{~V}$ | $\pm 37 \mathrm{~V}$ |  |
| Dimensions (excluding pin height) | $78.0 \mathrm{~mm} \times 44.0 \mathrm{~mm} \times 9.0 \mathrm{~mm}$ |  |  |

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## Specifications

Absolute maximum ratings at $\mathrm{Ta}=25^{\circ} \mathrm{C}$ (excluding rated temperature items), $\mathrm{Tc}=25^{\circ} \mathrm{C}$ unless otherwise specified

| Parameter | Symbol | Conditions | Ratings | Unit |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{H}}$ maximum quiescent supply voltage 1 | $\mathrm{V}_{\mathrm{H}}$ max (1) | When no signal | $\pm 95$ | V |
| $\mathrm{V}_{\mathrm{H}}$ maximum supply voltage 2 | $\mathrm{V}_{\mathrm{H}} \max (2)$ | $\mathrm{R}_{\mathrm{L}} \geq 6 \Omega, 150 \mathrm{~W}, 50 \mathrm{~ms}$ | $\pm 85$ | V |
| $\mathrm{V}_{\mathrm{L}}$ maximum quiescent supply voltage 1 | $\mathrm{V}_{\mathrm{L}} \max (1)$ | When no signal | $\pm 61$ | V |
| $\mathrm{V}_{\mathrm{L}}$ maximum supply voltage 2 | $\mathrm{V}_{\mathrm{L}} \max (2)$ | $\mathrm{R}_{\mathrm{L}} \geq 6 \Omega, 150 \mathrm{~W}, 50 \mathrm{~ms}$ | $\pm 55$ | V |
| Maximum voltage between $\mathrm{V}_{\mathrm{H}}$ and $\mathrm{V}_{\mathrm{L}}$ *4 | $\mathrm{V}_{\mathrm{H}^{-} \mathrm{V}_{\mathrm{L}} \text { max }}$ | No load | 60 | V |
| Thermal resistance | ${ }^{\text {ej-c }}$ | Per power transistor | 1.3 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| Junction temperature | Tj max | Both the Tj max and Tc max conditions must be met. | 150 | ${ }^{\circ} \mathrm{C}$ |
| IC substrate operating temperature | Tc max |  | 125 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | Tstg |  | -30 to +125 | ${ }^{\circ} \mathrm{C}$ |
| Allowable load shorted time *3 | ts | $\begin{aligned} & \mathrm{V}_{\mathrm{H}}= \pm 57 \mathrm{~V}, \mathrm{~V}_{\mathrm{L}}= \pm 38 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=6 \Omega, \mathrm{f}=50 \mathrm{~Hz} \\ & \mathrm{P}_{\mathrm{O}}=150 \mathrm{~W}, 1 \text {-channel active } \end{aligned}$ | 0.3 | s |

Electrical Characteristics at $\mathrm{Tc}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=6 \Omega, \mathrm{Rg}=600 \Omega, \mathrm{VG}=30 \mathrm{~dB}, \mathrm{VZ}=18 \mathrm{~V}$, non-inductive load $\mathrm{R}_{\mathrm{L}}$

| Parameter | Symbol | Conditions*1 |  |  |  |  |  | Ratings |  |  | unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{v}_{\mathrm{CC}}$ <br> (V) |  | $\begin{gathered} \mathrm{f} \\ (\mathrm{~Hz}) \\ \hline \end{gathered}$ | $\mathrm{PO}_{\mathrm{O}}$ <br> (W) | $\begin{gathered} \text { THD } \\ (\%) \\ \hline \end{gathered}$ |  | min | typ | max |  |
| Output power | $\mathrm{PO}_{\mathrm{O}}(1)$ | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 57 \\ & \pm 38 \end{aligned}$ | 20 to 20k |  | 0.7 |  | 150 |  |  | W |
| Total harmonic distortion | THD (1) | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 57 \\ & \pm 38 \end{aligned}$ | 20 to 20k | 150 |  |  |  | 0.4 |  | \% |
| Frequency characteristics | $\mathrm{f}_{\mathrm{L}}, \mathrm{f}_{\mathrm{H}}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 57 \\ & \pm 38 \end{aligned}$ |  | 1.0 |  | +0 -3dB |  | to 50 |  | Hz |
| Input impedance | ri | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 57 \\ & \pm 38 \end{aligned}$ | 1k | 1.0 |  |  |  | 55 |  | k $\Omega$ |
| Output noise voltage *2 | $\mathrm{V}_{\mathrm{NO}}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 68 \\ & \pm 46 \end{aligned}$ |  |  |  | $\mathrm{Rg}=2.2 \mathrm{k} \Omega$ |  |  | 1.0 | mVrms |
| Quiescent current | ${ }^{\text {I CCO }}$ | $\mathrm{V}_{\mathrm{H}}$ | $\pm 68$ |  |  |  |  |  |  | 70 |  |
|  |  | $\mathrm{V}_{\mathrm{L}}$ | $\pm 46$ |  |  |  |  |  |  | 100 |  |
| Output neutral voltage | $\mathrm{V}_{\mathrm{N}}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{H}} \\ & \mathrm{~V}_{\mathrm{L}} \end{aligned}$ | $\begin{aligned} & \pm 68 \\ & \pm 46 \end{aligned}$ |  |  |  |  | -70 | 0 | +70 | mV |

## [Remarks]

*1: Unless otherwise specified, use a constant-voltage power supply to supply power when inspections are carried out.
*2: The output noise voltage values shown are peak values read with a VTVM. However, an AC stabilized ( 50 Hz ) power supply should be used to minimize the influence of AC primary side flicker noise on the reading.
*3: Use the designated transformer power supply circuit shown in the figure below for the measurements of allowable load shorted time and output noise voltage.
*4: Design circuits so that $\left(\left|\mathrm{V}_{\mathrm{H}}\right|-\left|\mathrm{V}_{\mathrm{L}}\right|\right)$ is always less than 40 V when switching the power supply with the load connected.
*5: Set up the $\mathrm{V}_{\mathrm{L}}$ power supply with an offset voltage at power supply switching $\left(\mathrm{V}_{\mathrm{L}}-\mathrm{V}_{\mathrm{O}}\right)$ of about 8 V as an initial target.
*6: Weight of independent IC: 38.6 g
Package dimensions (length $\times$ width $\times$ height): $429 \mathrm{~mm} \times 245 \mathrm{~mm} \times 275 \mathrm{~mm}$


Designated transformer power supply (MG-250 equivalent)


Designated transformer power supply
(MG-200 equivalent)

## Package Dimensions

unit:mm (typ)


## Internal Equivalent Circuit



## Application Circuit Example



## Pin Assignments

STK412-150C-E PIN Assignment

| PIN No. | PIN Symbol | PIN Assignment |
| :---: | :---: | :---: |
| 1 | $+\mathrm{V}_{\mathrm{H}}$ | $+\mathrm{V}_{\mathrm{H}}$ Power Supply Voltage |
| 2 | $+\mathrm{V}_{\mathrm{L}}$ | + $\mathrm{V}_{\mathrm{L}}$ Power Supply Voltage |
| 3 | +Vref | +Side Shift Voltage Reference |
| 4 | -Vref | -Side Shift Voltage Reference |
| 5 | $-\mathrm{V}_{\mathrm{L}}$ | $-V_{L}$ Power Supply Voltage |
| 6 | $-\mathrm{V}_{\mathrm{H}}$ | $-\mathrm{V}_{\mathrm{H}}$ Power Supply Voltage |
| 7 | SUB GND | H-IC Sub GND |
| 8 | Ch1 +RE | Ch1 + Side Emitter Output |
| 9 | Ch1-RE | Ch1 -Side Emitter Output |
| 10 | Ch2-RE | Ch2 -Side Emitter Output |
| 11 | Ch1 +RE | Ch1 +Side Emitter Output |
| 12 | -Pre $\mathrm{V}_{\mathrm{H}}$ | -Side Pre. Supply Voltage |
| 13 | + Pre $\mathrm{V}_{\mathrm{H}}$ | +Side Pre. Supply Voltage |
| 14 | Ch1 IN | Ch1 Input |
| 15 | Ch1 NF | Ch1 Negative Feedback |
| 16 | Bias | Bias |
| 17 | Ch2 NF | Ch2 Negative Feedback |
| 18 | Ch2 IN | Ch1 Input |
| 19 | N.C. | No. Component |
| 20 | GND | GND |
| 21 | Ch2 FB | Ch2 Feedback for Protection |
| 22 | Ch1 FB | Ch1 Feedback for Protection |

## Sample PCB Trace Pattern



Parts List

| P.C.B. No. | STK412-150C-E/STK412-170C-E |
| :---: | :---: |
| R 01, 02 | $3.3 \mathrm{k} \Omega 1 \mathrm{~W}$ |
| R 03, 04 | 100 1W |
| R 05, 06, 18, 19, (07, 20) | $56 \mathrm{k} \Omega 1 / 6 \mathrm{~W}$ |
| R 08, 09, (10) | $4.7 \Omega 1 \mathrm{~W}$ |
| R 11, 12, (13) | 4.7 $\mathrm{I}^{1 / 4 \mathrm{~W}}$ |
| R 14, 15, (16) | $1.8 \mathrm{k} \Omega 1 / 6 \mathrm{~W}$ |
| R 17 | $33 \mathrm{k} \Omega 1 / 4 \mathrm{~W}$ |
| R 21, 22, (23) | $1 \mathrm{k} \Omega 1 / 6 \mathrm{~W}$ |
| R 24, 25, 26, 27, (28, 29) | $0.1 \Omega \pm 10 \% 5 \mathrm{~W}$ |
| C 01, 02, 05, 06 | 100 $\mathrm{F} / 100 \mathrm{~V}$ |
| C 03, 04 | 100 $\mu \mathrm{F} / 63 \mathrm{~V}$ |
| C 07, 08, (09) | 3 pF |
| C 10, 11, (12) | $0.1 \mu \mathrm{~F} / 100 \mathrm{~V}$ |
| C 13, 14, (15) | $100 \mu \mathrm{~F} / 10 \mathrm{~V}$ |
| C 16, 17, (18) | $2.2 \mu \mathrm{~F} / 50 \mathrm{~V}$ |
| C 19, 20, (21) | 470pF |
| C 22, 23, (24) | 220pF |
| L 01, 02, (03) | $3 \mu \mathrm{H}$ |
| D 01, 02 | GZA18Y (SANYO) |
| J 01, 02, 03, 07 | 10 mm |
| J 04, 05 | 12 mm |
| J 06, 10 | 17 mm |
| J 08, 09, 11, 12 | 14 mm |
| J 13 | 5 mm |
| J 14 | N.C |
| J 15 | 33mm |
| J 16 | 30 mm |
| J 17 | 5 mm |

## Evaluation Board Characteristics




Po-f




## Discontinued

## STK412-150C-E

[Thermal Design Example for STK412-150C-E]
The thermal resistance, $\theta \mathrm{c}-\mathrm{a}$, of the heat sink for total power dissipation, Pd , within the hybrid IC is determined as follows.
Condition 1: The hybrid IC substrate temperature, Tc, must not exceed $125^{\circ} \mathrm{C}$.
$\mathrm{Pd} \times \theta \mathrm{c}-\mathrm{a}+\mathrm{Ta}<125^{\circ} \mathrm{C}$
Ta: Guaranteed ambient temperature for the end product
Condition 2: The junction temperature, Tj , of each power transistor must not exceed $150^{\circ} \mathrm{C}$.
$\mathrm{Pd} \times \theta \mathrm{c}-\mathrm{a}+\mathrm{Pd} / \mathrm{N} \times \theta \mathrm{j}-\mathrm{c}+\mathrm{Ta}<150^{\circ} \mathrm{C}$
N : Number of power transistors
$\theta j$-c: Thermal resistance per power transistor
However, the power dissipation, Pd, for the power transistors shall be allocated equally among the number of power transistors.
The following inequalities result from solving equations (1) and (2) for $\theta \mathrm{c}-\mathrm{a}$.

$$
\begin{align*}
& \theta \mathrm{c}-\mathrm{a}<(125-\mathrm{Ta}) / \mathrm{Pd}  \tag{1}\\
& \theta \mathrm{c}-\mathrm{a}<(150-\mathrm{Ta}) / \mathrm{Pd}-\theta \mathrm{j}-\mathrm{c} / \mathrm{N}  \tag{2}\\
& \text { - Supply voltage } \quad \mathrm{V}_{\mathrm{H}}, \mathrm{~V}_{\mathrm{L}} \\
& \text { - Load resistance } \mathrm{R}_{\mathrm{L}} \\
& \text { - Guaranteed ambient temperature } \mathrm{Ta}
\end{align*}
$$

Values that satisfy these two inequalities at the same time represent the required heat sink thermal resistance.
When the following specifications have been stipulated, the required heat sink thermal resistance can be determined from formulas (1)' and (2)'.

## [Example]

When the IC supply voltage, $\mathrm{V}_{\mathrm{H}}= \pm 57 \mathrm{~V}, \mathrm{~V}_{\mathrm{L}}= \pm 38 \mathrm{~V}$ and $\mathrm{R}_{\mathrm{L}}$ is $6 \Omega$, the total power dissipation, Pd , within the hybrid IC, will be a maximum of 180 W at 1 kHz for a continuous sine wave signal according to the Pd-Po characteristics. For the music signals normally handled by audio amplifiers, a value of $1 / 8 \mathrm{P}_{\mathrm{O}}$ max is generally used for Pd as an estimate of the power dissipation based on the type of continuous signal. (Note that the factor used may differ depending on the safety standard used.)

This is:

$$
\mathrm{Pd} \approx 85 \mathrm{~W} \quad\left(\text { when } 1 / 8 \mathrm{P}_{\mathrm{O}} \text { max. }=19 \mathrm{~W}\right) .
$$

The number of power transistors in audio amplifier block of these hybrid ICs, N , is 4 , and the thermal resistance per transistor, $\theta \mathrm{j}$-c, is $2.1^{\circ} \mathrm{C} / \mathrm{W}$. Therefore, the required heat sink thermal resistance for a guranteed ambient temperature, Ta , of $50^{\circ} \mathrm{C}$ will be as follows.

From formula (1)'

$$
\begin{aligned}
\theta \mathrm{c}-\mathrm{a} & <(125-50) / 85 \\
& <0.88 \\
\theta \mathrm{c}-\mathrm{a} & <(150-50) / 85 \\
& <0.82
\end{aligned}
$$

From formula (2)' $\quad \theta \mathrm{c}-\mathrm{a}<(150-50) / 85-1.4 / 4$
Therefore, the value of $0.82^{\circ} \mathrm{C} / \mathrm{W}$, which satisfies both of these formulae, is the required thermal resistance of the heat sink.
Note that this thermal design example assumes the use of a constant-voltage power supply, and is therefore not a verified design for any particular user's end product.

## STK412-100 Series Stand-by Control \& Mute Control Application


*1 Metal Plate Cement Resistor $0.1 \Omega \pm 10 \%$ (5W)

## STK412-100 Series Load-Short \& DC Voltage Protect Application



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## STK412-150C-EISTK412-170C-E BTL Application



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[^0]:    *1 Metal Plate Cement Resistor $0.1 \Omega \pm 10 \%$ (5W)

