Secondary Side Synchronous Flyback Controller

The NCP4302 is a full featured controller and driver that provide all the control and protection functions necessary for implementing a synchronous rectifier operation in a flyback converter. With the use of the NCP4302, the space conscious flyback applications such as Adaptors, chargers, set top boxes can achieve significant efficiency improvements at minimal extra cost. In addition to the synchronous rectifier control, the IC incorporates an accurate TL431 type shunt regulator, current monitoring circuit and optocoupler driver to provide a single IC secondary solution. The NCP4302 works with any type of flyback topology (continuous mode, Quasi–resonant mode or discontinuous mode) – providing a high level of versatility.

Features

- Self-contained Control of Synchronous Rectifier in CCM, DCM, and QR Flyback Applications
- Interface to External Signal for CCM Mode
- True Secondary Zero Current Detection
- High Gate Drive Currents (2.5 A Source/Sink)
- High Voltage Operation
- Current Sense Flexibility (MOSFET R_{DS(on)} OR CS Resistor)
- Accurate Low Voltage Reference
 - NCP4302A 2.55 V, 1%
 - NCP4302B 1.275 V, 1%
- $\bullet\,$ Programmable Independent Secondary Side t_{on} and t_{off} Delays
- Maximum Frequency of Operation up to 250 kHz
- These are Pb-Free Devices

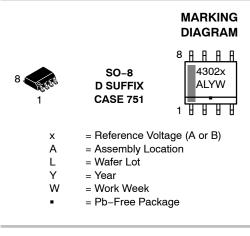
Typical Applications

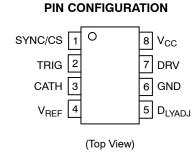
- Notebook Adapters
- LCD TV Adapters
- Consumer Appliances such as DVD, VCR
- Power Over Ethernet Applications (IP phones, Wireless Access Points)
- Battery Chargers



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ORDERING INFORMATION

Device	Package	Shipping [†]
NCP4302ADR2G	SO-8 (Pb-Free)	2500/Tape & Reel
NCP4302BDR2G	SO-8 (Pb-Free)	2500/Tape & Reel

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

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PIN DESCRIPTION

Pin Number	Symbol	Description
1	SYNC/CS	Connected to the flyback winding. The current on this pin is sensed and used to turn on the Synchronous Rectification MOSFET (SRFET). This pin is also used to sense the zero crossing of the MOSFET current either using the $R_{DS(on)}$ of the SRFET or using an external current sense resistor connected between drain of the SRFET and the flyback winding.
2	TRIG	Input pin for direct turn-off of the MOSFET. Typically connected to a signal from primary controller (for CCM mode) or a signal derived from the transformer (for QR mode). Has very short propagation delay to output (<50 ns).
3	CATH	Feedback compensation pin for the TL431 shunt regulator. Has the capability to sinking 10 ma of opto current.
4	V _{REF}	Output voltage feedback through resistive divider connected to this pin. Regulated at 1.28 V (option B) or 2.55 V (option A).
5	D _{LYADJ}	A resistive divider between the power supply output and ground with the center point tied to the D_{LYADJ} input pin allows for independent adjustment of the minimum t_{on} and t_{off} delay time. The maximum external capacitance from this pin to ground is 25 pF.
6	GND	Return pin for the controller – connected to the output return.
7	DRV	Drive output for external MOSFET – 2.5 A peak drive capability, internally clamped to 13.5 V (Maximum)
8	V _{CC}	Bias voltage for the controller. Maximum voltage is 28 V.

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Power Supply Input Current		-0.3 to 28 100	V mA
Drive Voltage Current	V _{DRV}	–0.3 to 18 100	V mA
Drive Current Source Sink	I _{DRV}	2.5 -2.5	Apk
Analog and Logic Inputs	TRIG, V _{REF} , D _{LYADJ}	–0.3 to 10 100	V mA
Maximum Voltage Current	SYNC/CS	– 10 to 95 100	V mA
Operating Junction Temperature Range	Т _Ј	-40 to 125	°C
Maximum Junction Temperature	T _{Jmax}	150	°C
Storage Temperature Range	T _{Smax}	-65 to 150	°C
Lead Temperature (Soldering, 10 s)	T _{Lmax}	300	°C
Reference input Current, continuous	I _{REF}	-0.05 to 10	mA
Total Power Dissipation	PD	225	mW
Thermal Resistance Junction-to-Ambient	θ_{JA}	178	°C/W

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.
1. This device series contains ESD protection and exceeds the following tests: Pin 1–8: Human Body Model 2000 V per JEDEC Standard JESD22, Method A114E. Machine Model (MM) 200 V per JEDEC Standard JESD22, Method A115A.
2. This device contains Latch-up protection and exceeds ±100 ma per JEDEC Standard JESD78

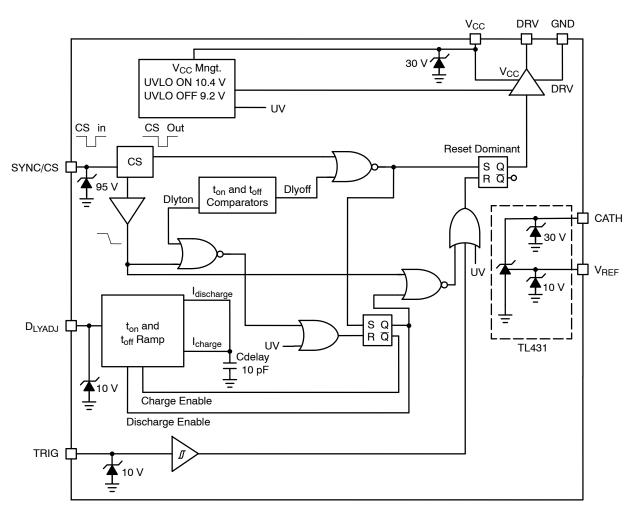


Figure 1. Block Diagram

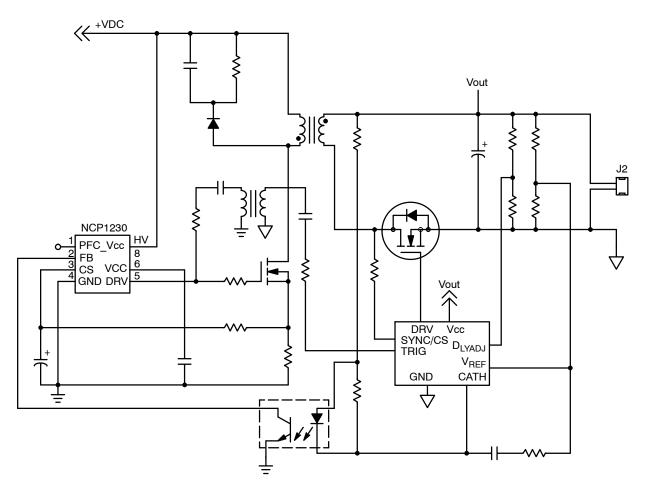


Figure 2. Typical Application

ELECTRICAL CHARACTERISTICS

 $(V_{CC} = 19 \text{ V}, \text{ Sync frequency} = 100 \text{ kHz}, V_{REF} = V_{KA} (I_{KA} = 1 \text{ mA}), R_S = 75 \text{ ohms}, V_{TRIG} = GND, C_{DRV} = 1 \text{ nF}, R_{DLYADJ} = 30.1 \text{ k}, V_{DLYADJ} = 2.0 \text{ V}, \text{ for typical values } T_J = 25^{\circ}\text{C}, \text{ for min/max values } T_J = -40^{\circ}\text{C} \text{ to } +125^{\circ}\text{C}, \text{ Max } T_J = 150^{\circ}\text{C}, \text{ unless otherwise noted})$

Rating	Test Conditions	Symbol	Min	Тур	Max	Unit
V _{cc}						
Start-up Threshold	V _{CC} ↑, SYNC/CS = 0 to −0.5 V 100 kHz, 5 μs pulse, Trig = 0 V	V _{CC(on)}	9.6	10.4	11.2	V
Stop Threshold	V _{CC} ↓, SYNC/CS = 0 to −0.5 V 100 kHz, 5 μs pulse, Trig = 0 V	V _{CC(off)}	8.5	9.2	-	V
V _{CC} shutdown Hysteresis	V _{CC(on)} – V _{CC(off)}	V _{CC(HYS)}	0.9	1.2	1.4	V
Supply current after turn-on	no–load on DRV pin, SYNC/CS = 0 to –0.5 V 100 kHz, 5 μs pulse, Trig = 0 V	I _{CC1}	-	2.7	5.6	mA
Supply current after turn-on	SYNC/CS = 0 to –0.5 V 100 kHz, 5 μs pulse, Trig = 0 V	I _{CC2}	Ι	3.6	7.5	mA
DRIVE OUTPUT						
Output voltage rise-time	10–90% of the output signal SYNC/ CS = 0 to –0.5 V 100 kHz, 5 μs pulse, Trig = 0 V	t _r	-	-	40	ns
Output voltage fall-time	10–90% of the output signal SYNC/ CS = 0 to –0.5 V, 100 kHz, 5 μs pulse, Trig = 0 V	t _f	-	-	40	ns
Output source current (Note 3)		I _{DRV(source)}	-	2.5	-	Apk
Driver high level output voltage	I_{SOURCE} = 200 mA, SYNC/CS = 0 to –0.5 V 100 kHz, 5 μs pulse, Trig = 0 V, V_{CC} = 12 V	V _{DRV(H)}	6.5	9.5	-	V
Output sink current (Note 3)		I _{DRV(sink)}	-	2.5	-	Apk
Driver Output low level output volt- age	I_{SINK} = 200 mA, SYNC/CS = 0 to –0.5 V 100 kHz, 5 μs pulse, Trig = 0 V, V_{CC} = 12 V	V _{DRV(L)}	-	160	500	mV
Drive voltage internal clamp	$\label{eq:V_CC} \begin{array}{l} V_{CC} = 28 \text{ V}, \ SYNC/CS = 0 \ \text{to} \ -0.5 \ V \\ 100 \ \text{kHz}, \ 5 \ \mu \text{s} \ \text{pulse}, \ \text{Trig} = 0 \ V, \\ DRVpin = 10 \ \mathrm{k}\Omega \end{array}$	V _{DRV(CLMP)}	-	-	17	V
Minimum drive output voltage	$\begin{array}{l} V_{CC}=V_{CC(off)}+200 \text{ mV, DRV pin}=\\ 10 k\Omega+1 \text{ nF, SYNC/CS}=0 \text{ to }-0.5 \text{ V}\\ 100 \text{ kHz, 5 } \mu \text{s pulse, Trig}=0 \text{ V} \end{array}$	V _{DRV(MIN)}	5.5	6.5	-	V
SYNC/CS						
The total propagation delay from SYNC/CS to the DRV output	$\begin{array}{l} SYNC/CS = +0.5 \ V \ to \ -0.5 \ V \ 100 \ kHz, \\ 5 \ \mu s \ pulse, \ (Trig = 0 \ V) (Refer \ to \ the \\ Drive \ Output \ specifications \ for \ Tr \ 50\% \\ of \ the \ output \ signal \end{array}$	t _{p1}	_	70	135	ns
Zero Current Detection	V _{SYNC/CS} < -30 mV	ls(zcd)	50	230	450	μA
Current Sense Pin Offset Voltage at Zero Current Level (Note 3)		VS(ZCD)	-30	-	-	mV
SYNC/CS Leakage current	V _{SYNC/CS} = 95 V	SCS _{Leakage}	_	-	10	μA
TRIGGER SECTION						
Minimum Trigger pulse duration	SYNC/CS = 0 to -0.5 V 100 kHz, 5 μ s pulse, Trig \uparrow	trig-pw	75	-	-	ns

Product parametric performance is indicated in the Electrical Characteristics for the listed test conditions, unless otherwise noted. Product performance may not be indicated by the Electrical Characteristics if operated under different conditions. 3. Guaranteed by Design

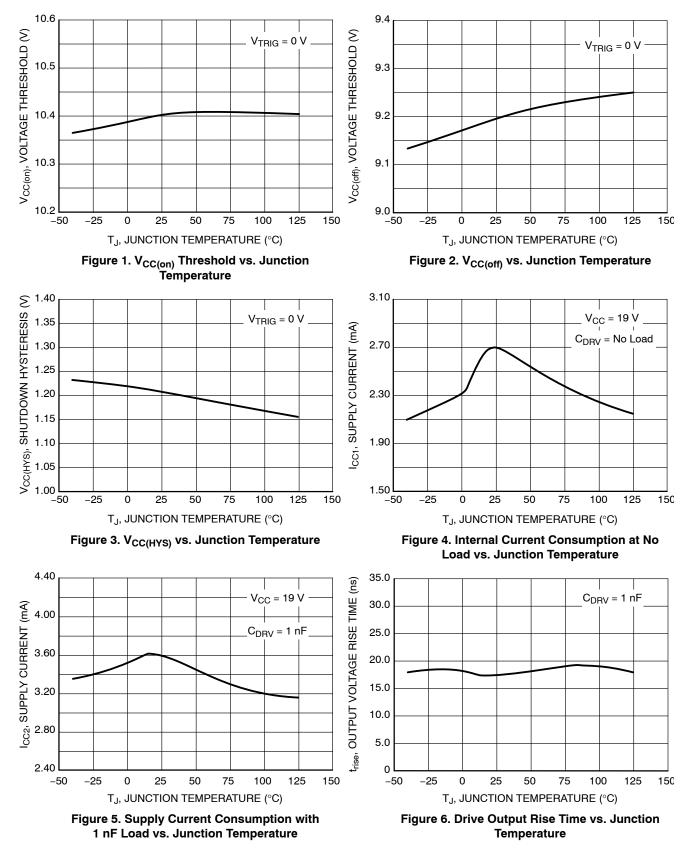
ELECTRICAL CHARACTERISTICS

 $(V_{CC} = 19 \text{ V}, \text{ Sync frequency} = 100 \text{ kHz}, V_{REF} = V_{KA} (I_{KA} = 1 \text{ mA}), R_S = 75 \text{ ohms}, V_{TRIG} = GND, C_{DRV} = 1 \text{ nF}, R_{DLYADJ} = 30.1 \text{ k}, V_{DLYADJ} = 2.0 \text{ V}, \text{ for typical values } T_J = 25^{\circ}\text{C}, \text{ for min/max values } T_J = -40^{\circ}\text{C} \text{ to } +125^{\circ}\text{C}, \text{ Max } T_J = 150^{\circ}\text{C}, \text{ unless otherwise noted})$

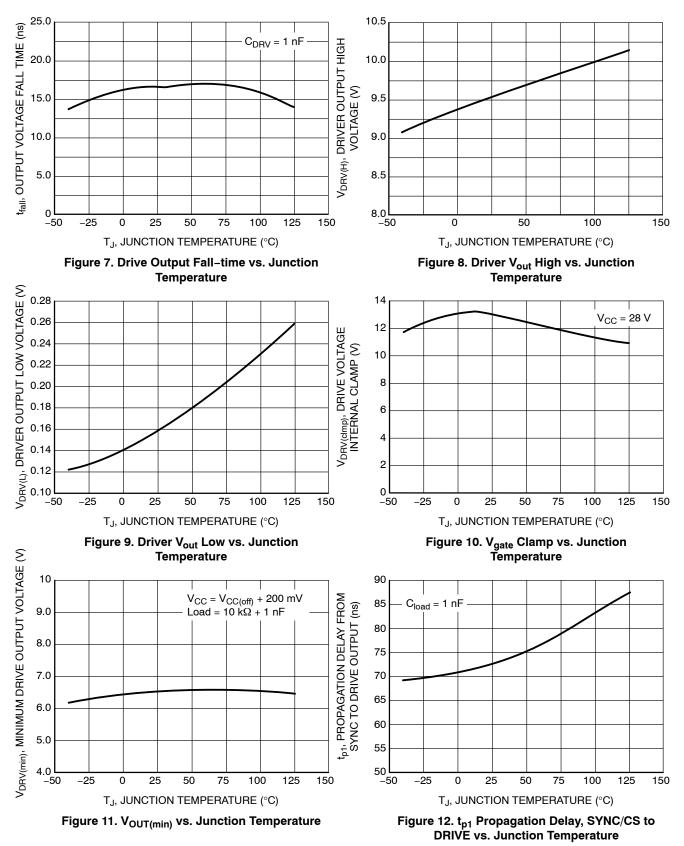
Rating	Test Conditions	Symbol	Min	Тур	Max	Unit
TRIGGER SECTION	•	•				
Trigger Pulse Voltage for Gate turn-off	SYNC/CS = 0 to -0.5 V 100 kHz, 5 μ s pulse, Trig \uparrow	Vtrig	2.0	_	4.0	V
Propagation delay from TRIG to DRV turn-off	C _{DRV} = no–load, SYNC/CS= –0.5 V 100 kHz, 5 μs pulse, Trig = 0–5 V ↑	t _{p2}	-	25	85	ns
TL431 CHARACTERISTICS	•	•		•	•	
Reference input voltage	I _{KA} = 5 mA, V _{KA} = V _{REF} NCP4302A	V _{REF}				V
	$T_{J} = +25^{\circ}C$ $T_{J} = -40^{\circ}C \text{ to } +125^{\circ}C$		2.525 2.499	2.55 -	2.575 2.60	
Reference input voltage	$(I_{K} = 5 \text{ mA}, V_{KA} = V_{REF})$ NCP4302B $T_{J} = +25^{\circ}C$ $T_{J} = -40^{\circ}C \text{ to } +125^{\circ}C$	V _{REF}	1.262 1.249	1.275 –	1.288 1.301	V
Reference Input Current	I _{KA} = 10 mA	I _{Ref}	-	0.0018	4.0	μΑ
Minimum CATH current for regulation	I _{SOURCE} [↑] 0 to 1 mA	I _{KA}	-	0.5	1.0	mA
Reference voltage line regulation	$\Delta V_{KA} = V_{CCon} - 16 \text{ V}, I_{KA} = 1 \text{ mA}$ $= \frac{\Delta V_{REF}}{\Delta V_{KA}}$	V _{KA}	_	2.0	5.0	mV/V
Off-State CATH Current	V_{KA} = 18 V, V_{REF} = 0 V (test circuit 2, V_{REF} pin grounded)	l _{Off}	-	11	20	μΑ
Dynamic impedance	$V_{KA} = V_{REF}$, $\Delta I_{KA} = 1$ mA to 10 mA	Z _{KA}	-	0.62	1.5	Ω
The maximum sink current capability	(I _{SOURCE} ↑ 0 to 10 mA)	Isinkmax	10	-	-	mA
ADJUSTABLE TIME DELAY						
The t _{on} time delay	$\begin{array}{l} SYNC/CS = 0 \mbox{ to } -0.5 \mbox{ V } 100 \mbox{ kHz}, 5 \mu s \\ \mbox{pulse, Trig = 0 V} \\ CD_{LYADJ} \mbox{ internal = 10 } pF \\ (Vs = 2.0 \mbox{ V, Rth = 30.1 } \Omega) \end{array}$	t _{on(delay)}	1.0	1.4	1.8	μs
The min and max t _{on(delay)} range (Note 3)	* R2 = 190 kΩ, R3 = 57 kΩ * R2 = 499 kΩ, R3 = 39 kΩ (*See Figure 27)	t _{on(range)}	0.45 -		_ 2.0	μs
The maximum and minimum input voltage operating range. (Note 3)	The maximum capacitance from pin 5 to ground is 25 pF.	Vin _{DLYADJ}	1.5	-	4.5	V
The maximum and minimum input operating current into the D _{LYADJ} pin (Note 3)		lin _{DLYADJ}	9	_	200	μΑ
The t _{off} time delay	$\begin{array}{l} SYNC/CS = 0 \mbox{ to } -0.5 \mbox{ V } 100 \mbox{ kHz}, 5 \mu s \\ \mbox{pulse, Trig = 0 V} \\ CD_{LYADJ} \mbox{ internal = 10 } pF \\ (Vs = 2.0 \mbox{ V, Rth = 30.1 } k) \end{array}$	t _{off(delay)}	2.8	3.8	4.8	μs
The min and max t _{off(delay)} range (Note 3)	R2 = 66 k, R3 = 23.6 k * R2 = 408 k, R3 = 32.4 k (*See the schematic below)	t _{off(range)}	0.8		_ 4.6	μs

Product parametric performance is indicated in the Electrical Characteristics for the listed test conditions, unless otherwise noted. Product performance may not be indicated by the Electrical Characteristics if operated under different conditions. 3. Guaranteed by Design



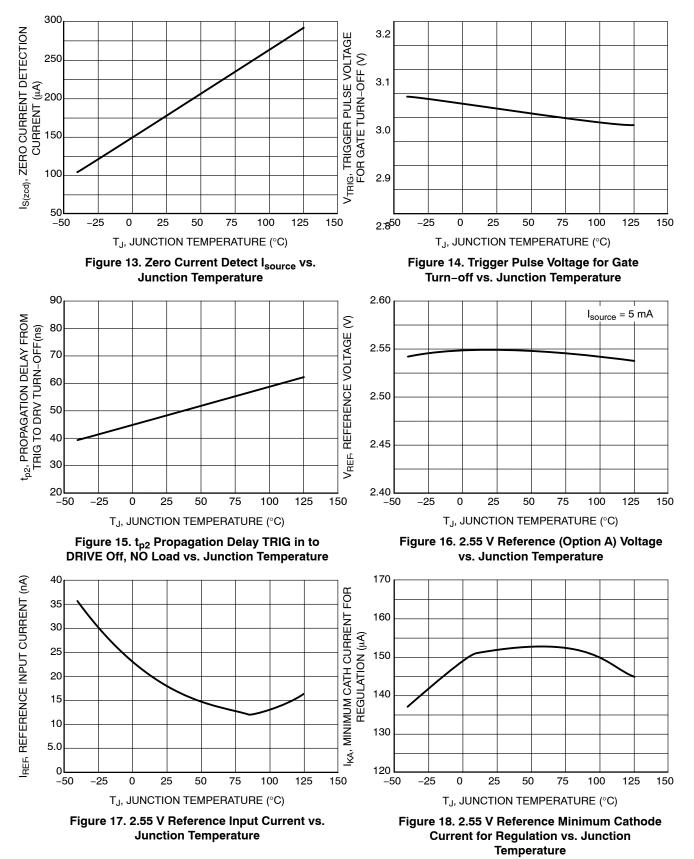


TYPICAL CHARACTERISTICS



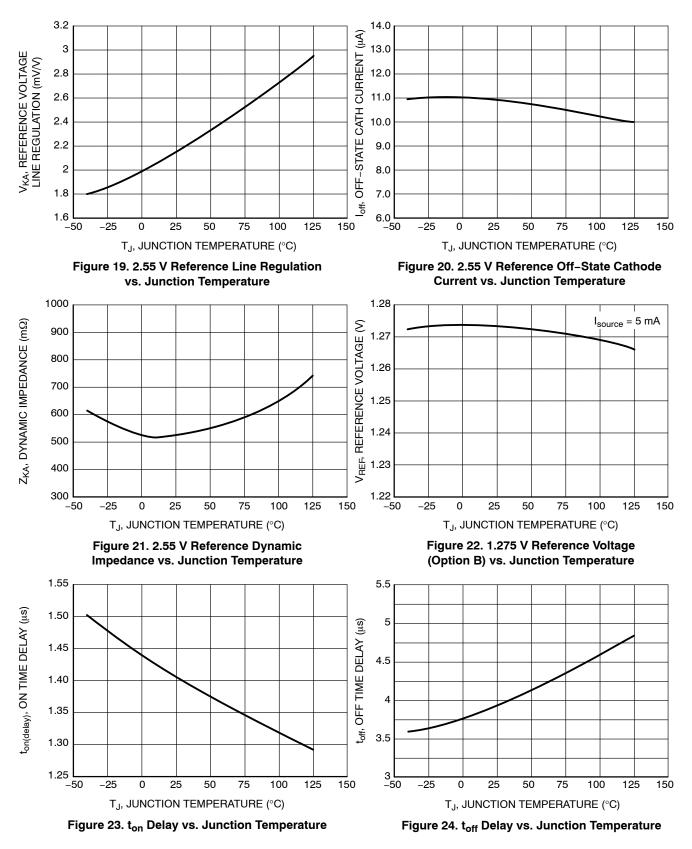
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TYPICAL CHARACTERISTICS



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TYPICAL CHARACTERISTICS



Detailed Operating Description

The NCP4302 is designed to operate either as a standalone IC or as a companion IC to a primary side controller to help achieve efficient synchronous rectification for flyback converter systems. It has high current gate driver along with fast logic circuitry to provide appropriately timed drive signals to a synchronous MOSFET used for output rectification in a flyback converter. With its novel architecture, the NCP4302 has enough versatility to increase the synchronous rectification efficiency under any operating mode without requiring too much complexity.

Supply Section

The NCP4302 works from an available bias supply that can range from 10.4 V to 28 V (typical). This allows direct connection to the output voltage of many adapters such as notebook and LCD TV adapters. As a result, the NCP4302 simplifies circuit operation compared to other devices which require specific bias power supplies (e.g. 5 V). The high voltage capability of the V_{CC} is also a unique feature designed to allow operation across a broader range of applications. To prevent gate signal from operating under inadequate bias conditions, the NCP4302 features a UVLO circuit that turns on at 10.4 V (V_{CC} rising) typical and turns off at 9.2 V typical (V_{CC} falling).

Gate Drive Section

The NCP4302 features high current gate drivers delivering up to (>2.5 A peak) to achieve fast turn-on and turn-off requirements in a synchronous rectifier. Having a high gate drive current enables fast turn-on when SYNC/CS signal is received (to minimize body diode conduction at the peak of the current waveform) and fast turn-off when zero current or a TRIG signals are received (to prevent current reversal or cross conduction). The higher sink current also allows the MOSFET to be kept off during the instances when there is high dv/dt on the drain.

The gate voltage is clamped at 13.5 V typical to prevent larger excursion of gate voltage than needed when V_{CC} is operating from a 28 Vdc output.

The propagation delays through the logic circuits and the gate drivers are kept at a minimum as shown in the specification table.

SYNC/CS Input

In a synchronous rectification application after the primary side MOSFET is turned-off, the current in the secondary of the flyback transformer initially flows through the synchronous rectification MOSFET's internal body diode. When this occurs, the drain of the MOSFET will be -0.5 to -1.0 V negative with respect to ground (the VF of the internal body diode) and the NCP4302 current sense differential amplifier will output a 230 μ A current (typical). This current detection method is used by the NCP4302 to determine when current is flowing in the secondary of the transformer and the Synchronous Rectification MOSFET needs to be turned-on.

The zero current detection senses the current with a slight negative offset so that the switch turn-off occurs without reversal of the current.

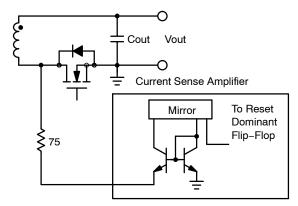
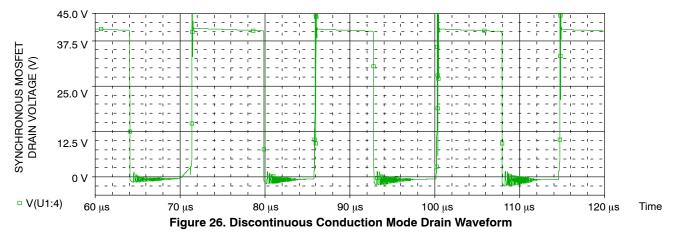


Figure 25. Input Current Sense

Adjustable ton Delay

The SYNC/CS input to the NCP4302 is used as a Reset (through logic) input to the drive enable Flip Flop; refer to the internal block diagram of the NCP4302. When current flows in the secondary of the Flyback transformer any parasitic inductance due to printed wiring board traces, or component lead can cause the voltage at the SYNC/CS input to ring above ground (refer to Figure 26). This ringing may cause the controller dive output to turn–off. To eliminate this problem the NCP4302 has a programmable t_{on} time which blanks the secondary voltage ringing by adding a minimum controller drive on time.



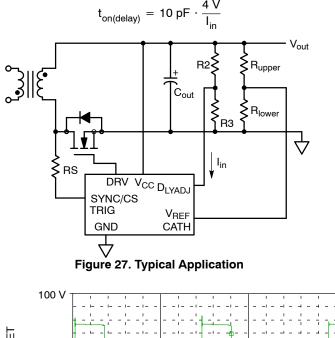
The minimum on time is set with a voltage divider with resistors R2 and R3 (refer to Figure 27).

$$I_{in} = \left(\left(V_{out} \cdot \frac{R3}{R3 + R2} \right) - 0.7 \right) \cdot \frac{1}{Rth}$$

Where Rth is the Thevenin equivalent resistance and is calculated by:

Rth =
$$\frac{1}{\frac{1}{R3} + \frac{1}{R2}}$$

This input current is then used to charge an internal 10 pF capacitor setting the minimum t_{on} time.



Adjustable toff Delay

The SYNC/CS input to the NCP4302 is used as the Set input to the drive enable Flip Flop; refer to the internal block diagram of the NCP4302. Refering to the SPICE simulations (Figure 28), you can see that when the system is operating under light load conditions the transformer secondary voltage rings below ground when the current reaches zero. When this occurs, the CS amplifier output may be falsely triggered providing a Set input to the Drive Flip Flop, turning on the output drive. To prevent the controller from prematurely turning on the synchronous rectification MOSFET, the output of the current sense amplifier is connected to a logic block with a programmable off time delay. The t_{off(delay)} can be independently programmed through the D_{LYADJ} pin.

$$\begin{split} I_{\text{in}} &= \left(\left(V_{\text{out}} \cdot \frac{\text{R3}}{\text{R3} + \text{R2}} \right) - 0.7 \right) \cdot \frac{1}{100\text{k}} \\ t_{\text{off(delay)}} &= 10 \text{ pF} \cdot \frac{3.35 \text{ V}}{I_{\text{in}}} \end{split}$$

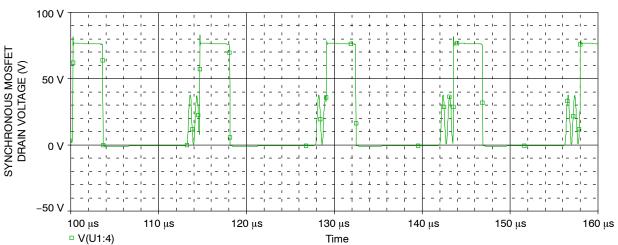


Figure 28. Discontinuous Conduction Mode Drain Waveform

Trigger Input

The TRIG input is used to turn-off the synchronous MOSFET prior to its current reaching zero. This input is required in a CCM operating mode. While there are several ways to determine the TRIG input, the simplest way is to generate a pulse in the primary side that precedes the turn-on of the primary MOSFET and transformer couple that pulse to the secondary into the Trig input. In converters where the operating mode is always designed to be DCM or QRM, the TRIG input is not used. It is recommended to ground the TRIG pin in these cases.

Voltage Amplifier and Reference

The NCP4302 incorporates an accurate TL431 type Shunt regulator with two reference voltage options. The NCP4302A has a 2.5 V reference and the NCP4302B has a 1.25 V reference.

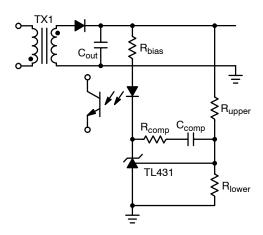


Figure 29. Typical Secondary Side Regulator

When the TL431 is being used to regulate the output of a power supply it is typically configured as shown in Figure 29. Where the output from the power supply is sensed and divided down with a resistive divider made up of R_{upper} and R_{lower} . The center point of the divider is connected to the reference pin of the NCP4302. The divider ratio scales down the output voltage to match the reference voltage, 2.5 V or 1.25 V.

$$V_{\mathsf{REF}} = V_{\mathsf{out}} \cdot \frac{\mathsf{R}_{\mathsf{lower}}}{\mathsf{R}_{\mathsf{lower}} + \mathsf{R}_{\mathsf{upper}}}$$

The R_{bias} resistor in Figure 29 sets the current through the TL431, which must be greater than 0.5 mA to guarantee its performance under all operating conditions.

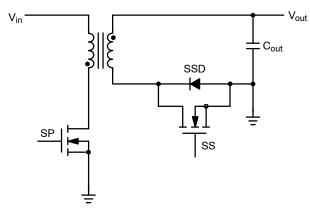


Figure 30. Synchronous Rectifier

Using Synchronous Rectification

For a flyback converter to operate correctly with synchronous rectification there must be a delay between the time when the primary side MOSFET (SP Figure 30) and the secondary side Synchronous rectification MOSFETs (SS Figure 29) are conducting current. The NCP4302 can operate in CCM, CRM, or QR modes. The next sections cover the losses associated for each of the three operating modes.

Discontinuous Conduction Mode

The basic switching waveforms for the Flyback converter operating in DCM are shown in Figure 31. When the primary side MOSFET (SP in Figure 30) is turned-on current flows is the transformer primary and ramps up from zero to I_{peak}. When the primary side MOSFET (SP) turns-off, the polarity of the transformer reverses and the energy stored in the transformer is transferred to the secondary. When the energy transfer from the transformer primary to the transformer secondary begins, (prior to the secondary side synchronous MOSFET turning-on) the secondary current flows through the internal body diode synchronous rectifiers MOSFETs (SS) and (SSD). To minimize the losses in the SSD, the propagation delay (t_{p1}) must be low. Otherwise, there will be high losses associated with the secondary peak current and the SSD forward voltage drop (NCP4302 has a typical propagation delay of 50 ns).

$$P_{Tsecondary} = P_{on} + P_{SW} + P_{diode}$$
 (eq. 1)

$$I_{out} = \frac{I_{sec,pk}}{2} \cdot (1 - D_{on}) \qquad (eq. 2)$$

$$I_{sec,rms} = I_{sec,pk} \cdot \sqrt{\frac{1 - D_{on}}{3}}$$
 (eq. 3)

Combining equations 2 and 3,

$$I_{\text{sec,rms}}^2 = \frac{4 \cdot I_{\text{out}}^2}{3 \cdot (1 - D_{\text{on}})} \quad (\text{eq. 4})$$

$$\mathsf{P}_{\mathsf{on}} = \frac{4 \cdot \mathsf{I}_{\mathsf{out}}{}^2}{3 \cdot (1 - \mathsf{D}_{\mathsf{on}})} \cdot \mathsf{R}_{\mathsf{DS}(\mathsf{on})} \tag{eq. 5}$$

$$\mathsf{P}_{\mathsf{SW}} = \frac{1}{2} \cdot \mathsf{C}_{\mathsf{OSS}} \cdot \mathsf{V}_{\mathsf{S}}^2 \cdot f \qquad (\mathsf{eq. 6})$$

$$\mathsf{P}_{\mathsf{diode}} = \mathsf{V}_{\mathsf{F}} \cdot \mathsf{I}_{\mathsf{out}} \cdot \mathsf{t}_{\mathsf{delay}} \tag{eq. 7}$$

Where:

Iout is the dc output current

V_F is

D is the duty cycle

R_{DS(on)} is the on resistance of the MOSFET

$$V_{S} = \frac{V_{in}}{n} + V_{out}$$

n is the transformer turns ratio T_{delay} is the delay from the sync to the drive output

Discontinuous Condition Mode

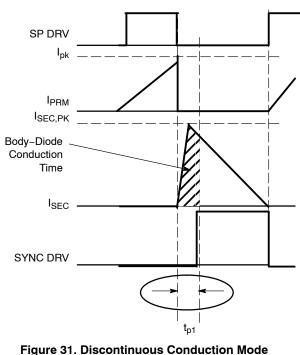


Figure 31. Discontinuous Conduction Mode Waveforms

 t_{p1} is the propagation delay from the SYNC/CS input to the drive output.

Continuous Conduction Mode

When operating in continuous conduction mode (CCM) the current in the secondary doesn't fall to zero prior to turning on the primary side MOSFET. To eliminate cross conduction losses (have the primary side MOSFET and secondary side MOSFET on at the same time) the trigger input to the NCP4302 must be utilized. A signal which leads the Primary Side (SP) MOSFET turning on must be coupled to the TRIG input of the NCP4302 which will turn-off the SS MOSFET referring to Figure 32.

When the energy transfer begins in the transformer secondary, prior to the secondary side synchronous MOSFET turning–on, the secondary current flows through the synchronous rectifiers MOSFET's (SS) internal body diode (SSD). To minimize the power loss in the internal body the controller propagation delay has been minimized in the NCP4302.

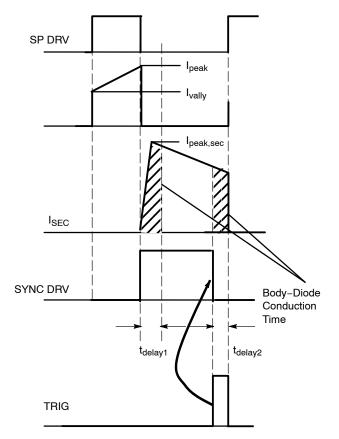


Figure 32. Continuous Conduction Mode Waveforms

$$P_{sync} = P_{ON} + P_{Qrr} + P_{d}P + PP_{OFF}$$
 (eq. 8)

$$I_{sec,RMS} \approx \left(I_{sec,peak} - \frac{\Delta I_{L_{sec}}}{2}\right) \sqrt{1 - D}$$
 (eq. 9)

$$I_{sec,RMS}^{2} \approx \left(I_{sec,peak}^{2} - \frac{\Delta I_{L_{sec}}^{2}}{2}\right)^{2} 1 - D \int (eq. 10)$$

Combining equations 9 and 10,

$$\Delta IL_{sec} = \frac{V_{OUT} + V_f}{\frac{LM}{n^2}} (1 - D)T \qquad (eq. 11)$$

$$P_{on} = I_{sec,RMS}^{2} \cdot R_{DS(on)}$$
 (eq. 12)

$$\mathsf{P}_{\mathsf{QRR}} = \mathsf{Q}_{\mathsf{RR}} \left(\mathsf{V}_{\mathsf{OUT}} + \frac{\mathsf{V}_{\mathsf{IN}}}{\mathsf{n}} \right) f \qquad (\mathsf{eq. 13})$$

 $\mathsf{P}_{\mathsf{BODY_DIODE}} = \mathsf{V}_f \cdot \mathsf{I}_{\mathsf{OUT}} \cdot f(\mathsf{t}_{\mathsf{delay1}} + \mathsf{td}_{\mathsf{delay2}}) \quad (\mathsf{eq. 14})$

$$\mathsf{P}_{\mathsf{off}} = \frac{1}{2} \cdot \mathsf{C}_{\mathsf{OSS}} \left(\mathsf{V}_{\mathsf{out}} + \frac{\mathsf{V}_{\mathsf{in}}}{\mathsf{n}} \right)^2 \cdot f \qquad (\mathsf{eq. 15})$$

 Q_{RR} is the recovery charge of the internal body diode Coss is the MOSFET drain to source capacitance L_M is the transformer primary inductance

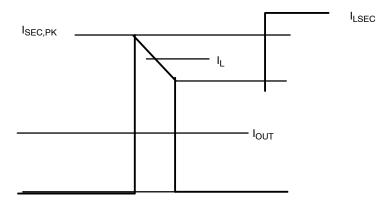


Figure 33.

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*For additional information on our Pb–Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

STYLES ON PAGE 2

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STYLE 1: PIN 1. EMITTER COLLECTOR 2. 3. COLLECTOR 4. EMITTER 5. EMITTER BASE 6. 7 BASE EMITTER 8. STYLE 5: PIN 1. DRAIN 2. DRAIN 3. DRAIN DRAIN 4. GATE 5. 6. GATE SOURCE 7. 8. SOURCE STYLE 9: PIN 1. EMITTER, COMMON COLLECTOR, DIE #1 COLLECTOR, DIE #2 2. З. EMITTER, COMMON 4. 5. EMITTER, COMMON 6 BASE. DIE #2 BASE, DIE #1 7. 8. EMITTER, COMMON STYLE 13: PIN 1. N.C. 2. SOURCE 3 GATE 4. 5. DRAIN 6. DRAIN DRAIN 7. DRAIN 8. STYLE 17: PIN 1. VCC 2. V2OUT V10UT З. TXE 4. 5. RXE 6. VFF 7. GND 8. ACC STYLE 21: PIN 1. CATHODE 1 2. CATHODE 2 3 CATHODE 3 CATHODE 4 4. 5. CATHODE 5 6. COMMON ANODE COMMON ANODE 7. 8. CATHODE 6 STYLE 25: PIN 1. VIN 2 N/C REXT З. 4. GND 5. IOUT IOUT 6. IOUT 7. 8. IOUT STYLE 29: BASE, DIE #1 PIN 1. 2 EMITTER, #1 BASE, #2 З. EMITTER, #2 4. 5 COLLECTOR, #2 COLLECTOR, #2 6.

STYLE 2: PIN 1. COLLECTOR, DIE, #1 2. COLLECTOR, #1 COLLECTOR, #2 3. 4 COLLECTOR, #2 BASE, #2 5. EMITTER, #2 6. 7 BASE #1 EMITTER, #1 8. STYLE 6: PIN 1. SOURCE 2. DRAIN 3. DRAIN SOURCE 4. SOURCE 5. 6. GATE GATE 7. 8. SOURCE STYLE 10: GROUND PIN 1. BIAS 1 OUTPUT 2. З. GROUND 4. 5. GROUND 6 BIAS 2 INPUT 7. 8. GROUND STYLE 14: PIN 1. N-SOURCE 2. N-GATE 3 P-SOURCE P-GATE 4. P-DRAIN 5 6. P-DRAIN N-DRAIN 7. N-DRAIN 8. STYLE 18: PIN 1. ANODE ANODE 2. SOURCE 3. GATE 4. 5. DRAIN 6 DRAIN CATHODE 7. CATHODE 8. STYLE 22 PIN 1. I/O LINE 1 2. COMMON CATHODE/VCC 3 COMMON CATHODE/VCC 4. I/O LINE 3 COMMON ANODE/GND 5. 6. I/O LINE 4 7. I/O LINE 5 8. COMMON ANODE/GND STYLE 26: PIN 1. GND 2 dv/dt З. ENABLE 4. ILIMIT 5. SOURCE SOURCE 6. SOURCE 7. 8. VCC STYLE 30: DRAIN 1 PIN 1. DRAIN 1 2 GATE 2 З. SOURCE 2 4 SOURCE 1/DRAIN 2 SOURCE 1/DRAIN 2 5.

6.

7.

8 GATE 1

SOURCE 1/DRAIN 2

STYLE 3: PIN 1. DRAIN, DIE #1 DRAIN, #1 2. DRAIN, #2 З. DRAIN, #2 4. GATE, #2 5. SOURCE, #2 6. 7 GATE #1 8. SOURCE, #1 STYLE 7: PIN 1. INPUT 2. EXTERNAL BYPASS THIRD STAGE SOURCE GROUND З. 4. 5. DRAIN 6. GATE 3 SECOND STAGE Vd 7. FIRST STAGE Vd 8. STYLE 11: PIN 1. SOURCE 1 GATE 1 SOURCE 2 2. З. GATE 2 4. 5. DRAIN 2 6. DRAIN 2 DRAIN 1 7. 8. DRAIN 1 STYLE 15: PIN 1. ANODE 1 2. ANODE 1 ANODE 1 3 ANODE 1 4. 5. CATHODE, COMMON CATHODE, COMMON CATHODE, COMMON 6. 7. CATHODE, COMMON 8. STYLE 19: PIN 1. SOURCE 1 GATE 1 SOURCE 2 2. 3. GATE 2 4. 5. DRAIN 2 6. MIRROR 2 7. DRAIN 1 MIRROR 1 8. STYLE 23: PIN 1. LINE 1 IN COMMON ANODE/GND COMMON ANODE/GND 2. 3 LINE 2 IN 4. LINE 2 OUT 5. COMMON ANODE/GND COMMON ANODE/GND 6. 7. 8. LINE 1 OUT STYLE 27: PIN 1. ILIMIT OVI O 2 UVLO З. 4. INPUT+ 5. 6. SOURCE SOURCE SOURCE 7. 8 DRAIN

DATE 16 FEB 2011

STYLE 4: PIN 1. 2. ANODE ANODE ANODE З. 4. ANODE ANODE 5. 6. ANODE 7 ANODE COMMON CATHODE 8. STYLE 8: PIN 1. COLLECTOR, DIE #1 2. BASE, #1 З. BASE #2 COLLECTOR, #2 4. COLLECTOR, #2 5. 6. EMITTER, #2 EMITTER, #1 7. 8. COLLECTOR, #1 STYLE 12: PIN 1. SOURCE SOURCE 2. 3. GATE 4. 5. DRAIN 6 DRAIN DRAIN 7. 8. DRAIN STYLE 16 EMITTER, DIE #1 PIN 1. 2. BASE, DIE #1 EMITTER, DIE #2 3 BASE, DIE #2 4. 5. COLLECTOR, DIE #2 6. COLLECTOR, DIE #2 COLLECTOR, DIE #1 7. COLLECTOR, DIE #1 8. STYLE 20: PIN 1. SOURCE (N) GATE (N) SOURCE (P) 2. 3. 4. GATE (P) 5. DRAIN 6. DRAIN DRAIN 7. 8. DRAIN STYLE 24: PIN 1. BASE EMITTER 2. 3 COLLECTOR/ANODE COLLECTOR/ANODE 4. 5. CATHODE 6. CATHODE COLLECTOR/ANODE 7. 8. COLLECTOR/ANODE STYLE 28: PIN 1. SW_TO_GND 2. DASIC OFF DASIC_SW_DET З. 4. GND 5. 6. V MON VBULK 7. VBULK 8 VIN

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7.

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COLLECTOR, #1

COLLECTOR, #1

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