

Circuit Note CN-0304

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	Devices Connected/Referenced	
	AD9834	75 MHz Complete Low Power DDS
	AD8014	400 MHz Low Power High Performance Amplifier

Low Power DDS Waveform Generator

EVALUATION AND DESIGN SUPPORT

Circuit Evaluation Boards

CN0304 Evaluation Board (EVAL-CN0304-SDZ) SDP-B Evaluation Board (EVAL-SDP-CB1Z)

Design and Integration Files

Schematics, Layout Files, Bill of Materials

CIRCUIT FUNCTION AND BENEFITS

The circuit shown in Figure 1 is a 75 MHz low power (25 mW total) direct digital synthesis (DDS) waveform generator. The output buffer and anti-imaging filter provide improved spectral performance, making it suitable for frequency generation or

clocking applications requiring sine wave, triangular wave, and square outputs up to 18 MHz.

Because they are sampled data devices, low power DDS devices must be followed by a suitable anti-imaging filter to remove spectral images. However, the maximum current output is approximately 4 mA into a recommended 200 Ω load; therefore, an optimum low power, low distortion op amp buffer at the DDS output provides a low impedance drive source for a high quality 50 Ω filter.

The combination of the DDS, output buffer, and seventh-order elliptic low pass filter provides high quality spectral performance.

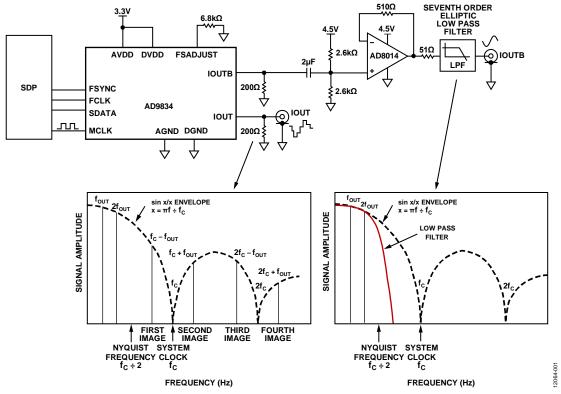


Figure 1. Low Power Waveform Generator (Simplified Schematic: All Connections and Decoupling Not Shown)

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CIRCUIT DESCRIPTION

The AD9834 is a 75 MHz complete low power (20 mW) DDS. It is designed to provide true and complementary current outputs up to 4 mA with output frequencies up to 37.5 MHz.

The AD8014 is a high speed current feedback amplifier with 400 MHz, -3 dB bandwidth, 4000 V/ μ s slew rate, and 24 ns settling time. It has extremely low voltage and current noise as well as low distortion. The low power (5.2 mW at +4.5 V), low cost, and 30 mA current drive capability make the AD8014 an attractive solution as a buffer for the AD9834 output. The circuit operates on +3.3 V for the AD9834 and +4.5 V for AD8014. The DDS operates with an SPI interface. The circuit consists of three blocks: the DDS block, the buffer block, and the low-pass filter block. Total power dissipation for the circuit is about 25 mW.

DDS Voltage Output

The full-scale adjust (FSADJUST) voltage and the external resistor, R_{SET} , determine the magnitude of the full-scale DAC current. The FSADJUST has a nominal value of 1.15 V, while the R_{SET} resistor has a typical value of 6.8 k Ω .

The full-scale current of the AD9834 is as follows:

$$I_{FULLSCALE} = 18 \times (FSADJUST/R_{SET})$$

This circuit uses a specified load of 200 Ω and maximum full-scale current to achieve voltage output without exceeding the compliance range of the DAC.

$$I_{FULLSCALE} = 18 \times (1.15/6800~\Omega) = 3~mA,$$

$$V_{OUT} = 3~mA \times 200~\Omega = 0.6~V$$

There are two current outputs available on the board: IOUT and IOUTB. The IOUT is unfiltered, and the IOUTB is filtered.

Buffer Amplifier

Due to the limited current and voltage compliance range at the output of the DDS, a buffer is necessary to provide higher current drive capability to the low-pass filter. In addition, the buffer provides isolation between the DDS block and the filter block and converts the 200 Ω output impedance of the loaded DDS to the 50 Ω required to drive the terminated filter. In this circuit note, the low-power high-performance current feedback operational amplifier AD8014 is used as an output buffer of the AD9834. The AD8014 is a high speed current feedback amplifier with 400 MHz, -3 dB bandwidth, 4000 V/ μ s slew rate and 24 ns settling time. It has an output current drive of \geq 30 mA. The feedback resistor in the AD8014 current feedback op amp sets the bandwidth of the op amp.

Figure 2 shows the feedback resistor of 510 Ω . Because the op amp is operating from a single polarity supply, the output needs to be centered on mid-supply to prevent clipping. The voltage divider at point A provides a 2.25 V dc offset to the sinusoidal signal that gives an output swing of 2.25 V \pm 0.3 V. For correct biasing of op amps in single supply applications, refer to Application Note AN-581, *Biasing and Decoupling Op Amps in Single Supply Applications*. For more information on current

feedback amplifiers, refer to the MT-034 Tutorial, *Current Feedback (CFB) Op Amps*.

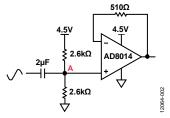


Figure 2. AD8014 Input and Feedback Connections

Seventh-Order Elliptic Low Pass Filter

The anti-imaging reconstruction must attenuate the image frequencies inherent to a sampled system as shown in Figure 1.

There are four basic filter types that can be used as a reconstruction filter: Cauer (elliptic), Chebyshev, Butterworth, and Bessel. Figure 3 shows the response curves of these four basic filter types.

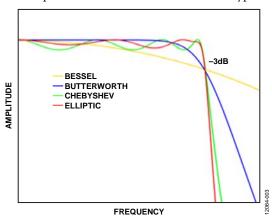


Figure 3. Response Curves for Four Basic Filter Types

For the same order, the elliptic filter has a higher roll-off rate compared to the other three, therefore, it makes an attractive candidate for the reconstruction filter. The filter used in this circuit note is a $7^{\rm th}$ order elliptic filter with a -3 dB bandwidth of 18 MHz.

Component Selection

The resistors, capacitors, and inductors used to implement the filter are passive components, and, due to the high frequencies involved, must meet the following requirements:

- Low parasitic capacitance and inductance.
- Low tolerance values so that the measured response is close to the design response.
- Wide temperature range.
- Small physical to minimize parasitic capacitance and inductance.

These are just a few of the criteria that ensure measured filter response is close to the simulated filter response.

For more information on selecting passive components for specific application, please refer to Basic Linear Design: Chapter 10, Passive Components.

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Filter Design and Performance

The 7th order elliptic filter is shown in Figure 4, and the simulated and actual frequency response of the filter is shown in Figure 5. The software used is Advances Design System (ADS) Version 2012.08. The actual filter components and manufacturers can be found in the bill-of-materials in the CN0304 Design Support Package at

http://www.analog.com/CN0304-DesignSupport.

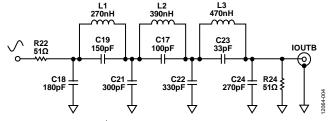


Figure 4. 7th order, Shunt-Connected Low Pass Filter

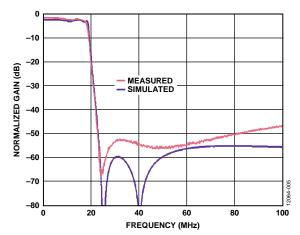


Figure 5. Simulated vs. Measured Frequency Response of the 7th-Order Elliptic Filter

The measured filter response was taken using the Agilent E5061B Network Analyzer. It shows the -3 dB bandwidth to be 18 MHz. The pass band attenuation is approximately 6 dB due to the source and load termination.

To check the performance of the circuit, the spectrum of the DDS output were measured with AD9834 set to an output frequency of 15 MHz with a 75 MSPS clock. The unfiltered and filtered outputs are shown in Figure 6 and Figure 7, respectively.

As shown in Figure 7, there is a significant reduction of the undesired images that appear in the unfiltered spectrum of Figure 6. The highest image spur at 60 MHz is suppressed by about 52 dB relative to the unfiltered output. This corresponds to the measured attenuation of the filter at 60 MHz.

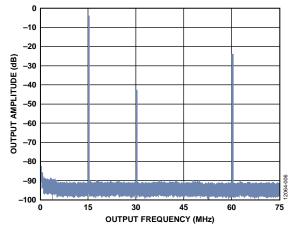


Figure 6. Unfiltered Output of AD9834 set to 15 MHz measured at IOUT

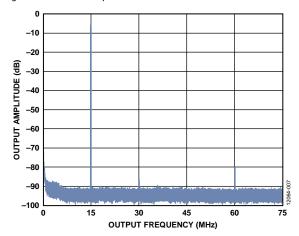


Figure 7. Filtered Output of AD9834 set to 15 MHz taken at IOUTB

The 600 mV p-p output of the AD9834 is attenuated by approximately 6 dB by the filter, and an additional 1 dB by the sin x/x roll off. The output into the 50 Ω load is therefore approximately 268 mV p-p, or 94.7 mV rms. This corresponds to 0.179 mW, or –7.5 dBm.

For more information on the reconstruction filter design for DDS, refer to Application Note AN-837, *DDS-Based Clock Jitter Performance vs. DAC Reconstruction Filter Performance*.

The circuit must be constructed on a multilayer PC board with a large area ground plane. Proper layout, grounding, and decoupling techniques must be used to achieve optimum performance (see MT-031 Tutorial, *Grounding Data Converters and Solving the Mystery of "AGND" and "DGND*," and MT-101 Tutorial, *Decoupling Techniques*).

Complete design support package including schematics, layouts, and bill of materials can be found at http://www.analog.com/CN0304-DesignSupport.

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COMMON VARIATIONS

An alternative for the DDS is the AD9838. It has lower power (11 mW) and offers the same functionality of the AD9834 but with lower clock rate of 16 MHz.

The buffer used in this circuit note is the current-feedback amplifier AD8014. An alternative for this is the ADA4860-1. It is a low cost, high speed (800 MHz, -3 dB bandwidth), low power (22.5 mW at 5 V), current feedback operational amplifier, but with a lower slew rate of 790 V/ μ s.

A voltage-feedback (VFB) amplifier can also be used for the buffer. The advantage of a VFB amplifier is lower noise and more freedom in choosing feedback components. The AD8057 is a voltage feedback amplifier with bandwidth and slew rate normally found in current feedback amplifiers. It has 325 MHz, $-3\ dB$ bandwidth, gain flatness of 0.1 dB to 28 MHz, and slew rate of 1000 V/ μs .

Another alternative is the ADA4897-1. It is a unity-gain stable, low wideband noise, rail-to-rail output high speed voltage feedback amplifier, with input voltage noise of 2.4 nV/ $\sqrt{\text{Hz}}$ at 10 Hz and a spurious free dynamic range (SFDR) of -80 dBc at 2 MHz.

The ADA4851-1 can also be used as buffer. It is a low cost, low power, high-speed (-3 dB bandwidth of 130 MHz) device, but with much a lower slew rate of 375 V/ μ s.

CIRCUIT EVALUATION AND TEST

Equipment Required

- EVAL-CN0304-SDZ evaluation board
- EVAL-SDP-CB1Z evaluation board
- AD9834 Evaluation Software
- Agilent E3631A triple output dc power supply or equivalent
- Rohde and Schwarz FSUP50 Signal Source Analyzer
- Agilent E5061B Network Analyzer (needed only to evaluate the filter response)

Filter Response Measurement

The frequency response of the filter was measured with a network analyzer using the setup shown in Figure 8.

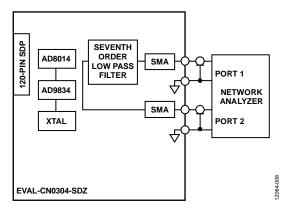


Figure 8. Test Setup for Measuring Filter Response

The EVAL-CN0304-SDZ board was modified, and the signal from the network analyzer applied to the input of the filter. The output of the filter was connected to the second port of the analyzer.

Output Waveform Measurement

The output waveform of the DDS was measured using the setup in Figure 9.

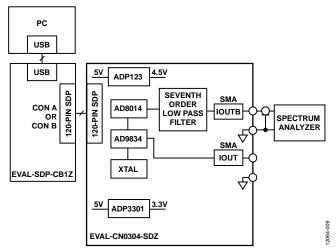


Figure 9. Test System Functional Diagram for DDS Output

The 5 V supply for the EVAL-CN0304-SDZ is derived from the 5 V USB voltage from the SDP card. Set the jumpers as follows: LK1 in B position, LK2 in B position, and LK3 removed.

The AD9834 Evaluation Software, located at ftp://ftp.analog.com/pub/evalcd/AD9834/, was used to set the output frequency and amplitude of the DDS. See the AD9834 Evaluation Board User Guide, UG-266 for further details. The hardware described in UG-266 does not have the 7th order output filter; however, the graphical user interface and software operation is identical to the EVAL-CN0304-SDZ hardware.

A photograph of the CN0304 printed circuit board is shown in Figure 10.

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Figure 10. Photograph of the EVAL-CN0304-SDZ Board

LEARN MORE

CN0304 Design Support Package: http://www.analog.com/CN0304-DesignSupport.

ADIsimDDS Design and Evaluation Tool.

UG-266 User Guide, Evaluating the AD9834 20 mW Power, 2.3 V to 5.5 V, 75 MHz Complete DDS. Analog Devices, Inc., 2011.

Kester, Walt. Chapter 3, Chapter 7, and Chapter 8, *The Data Conversion Handbook*. Analog Devices, Inc., 2005.

MT-015 Tutorial, *Basic DAC Architectures II: Binary DACs*. Analog Devices, Inc.

MT-031 Tutorial, *Grounding Data Converters and Solving the Mystery of AGND and DGND*. Analog Devices, Inc.

MT-034 Tutorial, *Current Feedback (CFB) Op Amps*. Analog Devices, Inc.

MT-085 Tutorial, Fundamentals of Direct Digital Synthesis (DDS). Analog Devices, Inc.

MT-101 Tutorial, Decoupling Techniques. Analog Devices, Inc.

David Brandon and Ken Gentile. AN-837 Application Note, DDS-Based Clock Jitter Performance vs. DAC Reconstruction Filter Performance. Analog Devices, Inc.

Riordan, Liam. AN-1070 Application Note, *Programming the AD9833/AD9834*. Analog Devices, Inc.

Data Sheets and Evaluation Boards

AD9834 Data Sheet.

AD8014 Data Sheet.

REVISION HISTORY

4/14—Revision 0: Initial Version

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